212D6212 **TEKNIK PELEDAKAN**

UNIVERSITAS HASANUDDIN

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1. Use Forms of Explosives

- 2. Estimating Properties of Explosives
- 3. Explosive Selection Criteria
- 4. Blasting Accessories
- 5. Initiation and Priming Systems



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- 6. Nonelectric Initiators
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16.Bench Blasting 17. Drilling Patterns and Hole Sequencing **18. Initiation Sequence and Delay Timing** 19. Explosives as a Source of Fragmentation Energy

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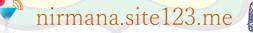
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23. Perimeter/Contour and Controlled Blasting

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Estimating Properties of **Explosives**

RIOGEI https://www.miningmagazine.com/supply-chainmanagement/news/1371861/riogel-causing-latam-blast





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Properties of Explosives

- 1. Strength and Energy
- 2. Cohesiveness
- 3. Detonation Velocity (VOD)
- 4. Density
- 5. Detonation Pressure and Explosion Pressure
- 6. Borehole Pressure



Properties of Explosives

Stability 7.

- Water Resistance 8.
- 9. Sensitivity
- 10. Detonation Transmission
- 11. Desensitization
- 12. Temperature Resistance



Properties of Explosives

- 13. Fumes
- 14. Inflammability
- 15. Safety in Handling
- 16. Storage Qualities
- 17. Medical Aspects
- 18. Permissibility



Introduction Conventional explosives and blasting agents

have different properties which characterize them and are used in assessing them for correct selection, depending upon the type of blasting to be carried out and the conditions under which it will be put into operation.



The selection of the type of explosive to be used for a particular task is based on 2 (two) primary criteria.

- 1. The explosive must be able to function safely reliably under the environmental and conditions of the proposed use.
- 2. The explosive must be the most economical to use to produce the desired end result.





Before any blaster selects an explosive to be used for a particular task, one must determine which explosives would best suit the particular environment and the performance characteristics which will suit the economy of the job.



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Hence, it is appropriate that knowledge about properties of explosives is obtained so that type and quantity of explosives used can be decided based on its ability to function under the specified conditions and achieve the objectives efficiently.

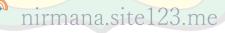
The properties of each group of explosives

also give prediction of the probable results of

fragmentation, displacement, and

vibrations.

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The most important characteristics are: strength and energy developed, detonation velocity (VOD), density, detonation pressure, water resistance, and sensitivity. Other properties which affect their use and must be taken into account are: fumes, temperature resistance, desensitivation by external causes, etc.





Numerous other properties can be specified for explosives but have not been included here because of their lack of importance to the field blaster.





From the industrial application point of view, the strength is one of the most important properties as it defines the energy available to produce mechanical effects. Strength refers to the energy content of an explosive which in turn is the measure of the force it can develop and its ability to do work.



There are different terms to express the strength of an explosive. In the original dynamites (straight dynamite), the percentage of nitroglycerin was the parameter to measure the strength.



Later, with the partial substitution of nitroglycerin with other products and the carrying out of comparative laboratory tests, the terms were changed to **Relative Weight Strength** and Relative Bulk Strength.



This way, it is frequent to refer to the strength of an explosive in so much percent of another taken as a standard, such as pure gelatin dynamite, ANFO, etc., which has the assigned value of 100.



There is no standard strength measurement method universally used by the explosives manufacturers.

Strength ratings are *misleading* and *do not* accurately compare rock fragmentation effectiveness with explosive type.





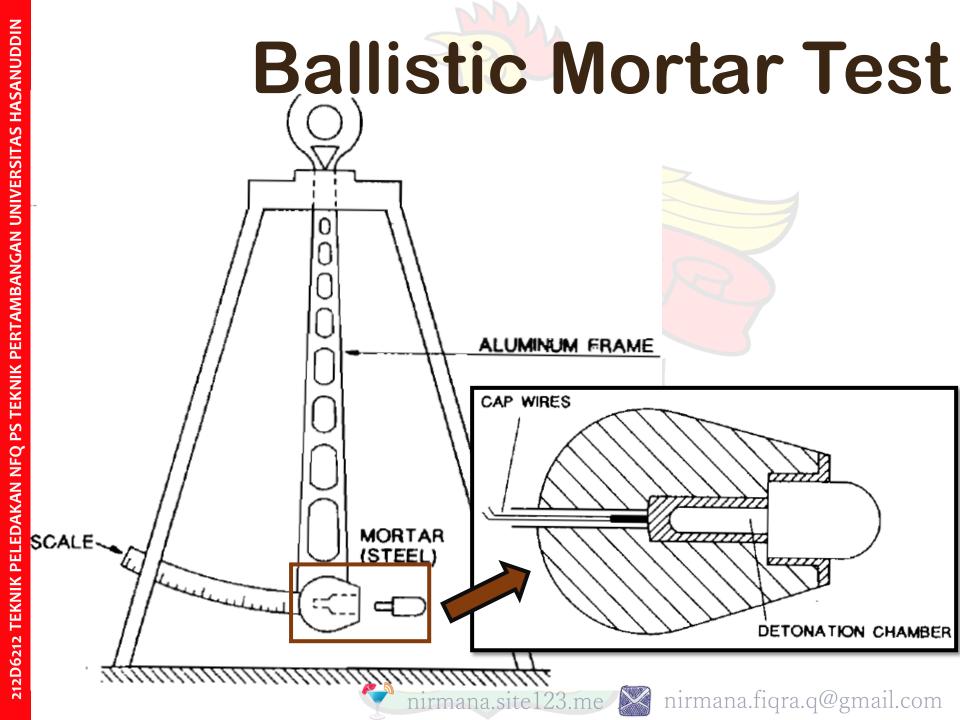
There are various practical 4. Crater charges test methods to measure the Cylinder compression 5. strength or the available test energy of an explosive.

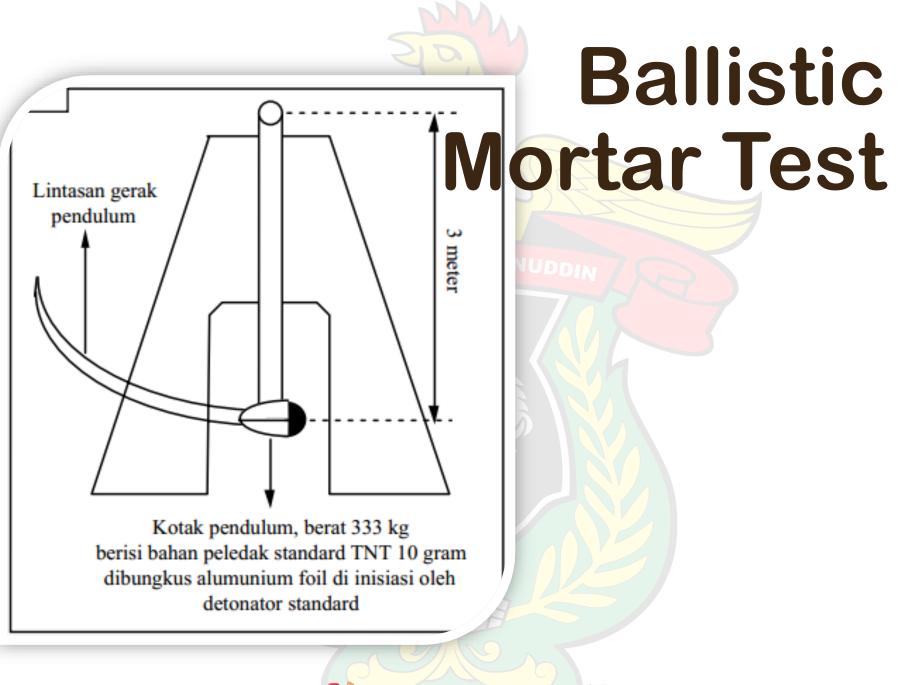
- Traulz test 1.
- 2. Ballistic mortar test
- 3. Seismic Strength test

- 6. Plate dent method
- 7. Double pipe test
- **Underwater test** 8
- **Empirical** equations 9.











Ballistic Mortar Test

This consists in comparing the propulsion of a steel mortar mounted upon a ballistic pendulum by the effect of the gases when a charge of 10 g of explosive is detonated.



Ballistic Mortar Test

The T.B.M. index is calculated from the equation:

$$T.B.M. = 100 \times \frac{1 - \cos \alpha}{1 - \cos \beta}$$

where α and β are the angles registered in the recoil deflection of the pendulum corresponding to the test explosive and the standard explosive.





Underwater tests have been used to determine the shock energy and expanding gas energy of an explosive. These two energy values have been used quite successfully by explosive manufacturers in predicting the capability of an explosive to break rock.



Underwater tests have been found to be useful tool in evaluating relative strengths of various explosives provided that these tests are carefully interpreted in conjunction with theoretical calculations and field performance.

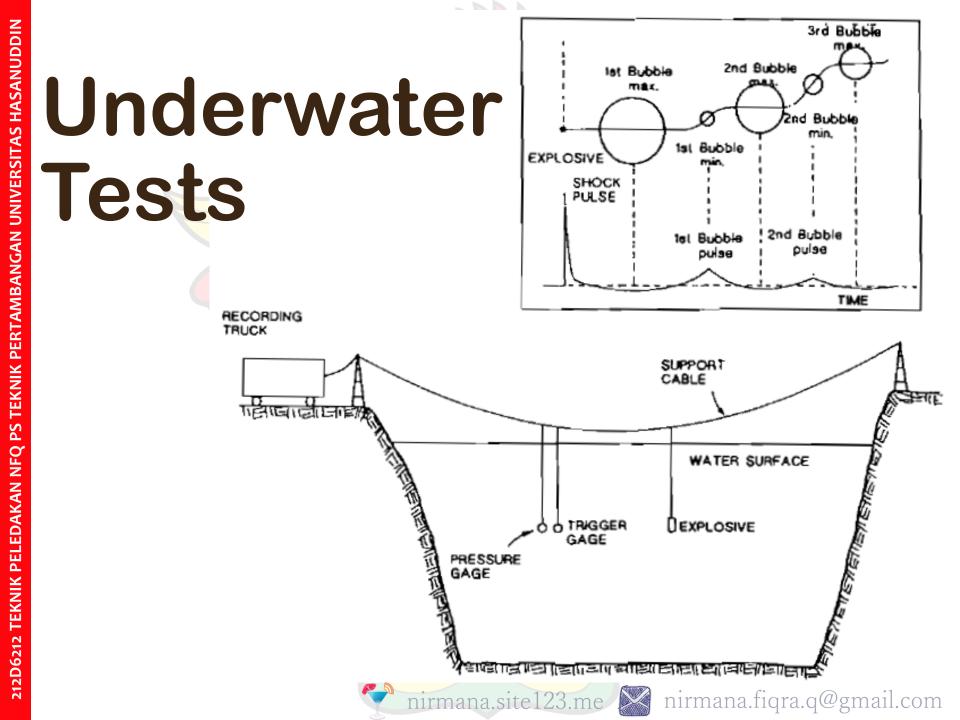


This technique to quantify energy released by an explosive was suggested by Cole in 1950s, and it is characterized as being one of the most complete as it permits tests with charge geometries similar to those in blastholes.



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Another feature is that it permits the separate calculation of the energy linked to the strain wave (Strain Energy-ET) and the energy of the detonation gases (Bubble Energy-EB), as well as the possibility of evaluating the influence of the initiation system on the energy released by an explosive.



Experience has shown that bubble energy values frequently overrate an explosive's ability to fragment hard rock, but are more closely related to the capability of displacing weak rock.



This method is very useful for comparing the yields of similar explosives under the same testing conditions. At the moment, it is the most used procedure in evaluating explosive energy, because with exception of the Thermic Energy, the rest is reliably assessed.





Empirical Equations

The equation used to calculate the Relative Weight Strength is

$$PRP = \left(\frac{\rho_e \times VD^2}{\rho_o \times VD_o^2}\right)^{1/3}$$

where ρ_e = density of the explosive (g/cm³),

VD = detonation velocity (m/s), ρ_o and VD_o refer to the standard explosive.



1. Strength and Energy

Even these new tests and calculations, when considered independently of one another, do not predict an explosive's effectiveness in all cases. To date, no single test or calculation can predict the blasting action of a commercial explosive, principally because of the complex nature of the materials being blasted.



1. Strength and Energy

performance of an explosive is The not determined simply by knowing the total energy released by the explosive. It depends also upon the rate of energy release and how effectively the energy is utilized in fragmenting and moving the material being blasted.





1. Strength and Energy

the explosive properties and the Both properties of the material being blasted

influence the effectiveness of an explosive.





Theoretical Energy

1. Heat of Explosion, Q

This energy represents the <u>total thermal energy</u> and includes the heat retained by products of detonation at atmospheric pressure.

2. Expansion Work (EWK)

<u>The energy</u> of the detonation products which be examined <u>at</u> <u>different temperature and pressure states of expansion,</u> <u>ending with gas expansion</u> to atmospheric pressure.



Theoretical Energy

In some cases, however, EWK may be higher than Q because of the change in reaction products with expansion.

Energy tied up in the expanded detonation products is *not a useful blast energy*.



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2. Cohesiveness

Cohesiveness is defined as the ability of the

explosive to maintain its original shape.





Detonation velocity refers to the speed with which the detonation wave İS propagated through the explosive and, therefore, is the parameter which defines the rhythm of energy release.



It ranges from about 5,500 to 25,000 fps (1 ft = 0.3048 meters, hence it ranges from about 1,676 to 7,620 meters) for products used commercially today.





A high detonation velocity gives the shattering action that many experts feel is necessary for difficult blasting conditions, whereas low-velocity products are normally adequate for the less demanding requirements typical of most blasting jobs.





Detonation velocity, particularly in modern dry blasting agents and slurries, may vary considerably depending on field conditions.





- The factors that affect VOD are:
- ✓ charge density,
- ✓ diameter,
- \checkmark confinement,



✓ initiation or priming It is essential that adequate priming is ensured so that the explosive may reach its maximum velocity as quickly as possible. Inadequate priming can result in the failure of the explosive to detonate, a slow build-up to final velocity, or a velocity detonation (which amounts to low deflagration); nirmana.site123.me 🔀 nirmana.fiqra.q@gmail.com

✓ aging of the explosive

(the process of change in the properties of a occurring over a material period, either spontaneously or through deliberate action).



Detonation velocity can often be increased by

the following:

- 1. Using a larger charge diameter.
- 2. Increasing density (although excessively high densities in blasting agents may seriously reduce sensitivity).



- 3. Decreasing particle size (pneumatic injection of AN-FO in small diameter boreholes accomplishes this).
- 4. Providing *good confinement* in the borehole.





- 5. Providing a high coupling ratio (coupling ratio is the percentage of the borehole diameter filled with explosive).
- 6. Using a *larger initiator or primer* (this will increase the velocity near the primer but will not alter the steady state velocity).



There is a difference of opinion among experts as to how important detonation velocity is in the fragmentation process. It probably is of *some* benefit in propagating the initial cracks in hard, massive rock. In the softer, prefactured rocks typical of most operations, it is of *little*

importance.



Velocity determinations are made by measuring the time required for the detonation wave to measured distance longitudinally travel a through a column of the explosive.





- There are diverse methods to measure VOD, among which the following are emphasized:
- D'Autriche method
- Kodewimetro
- Chronograph





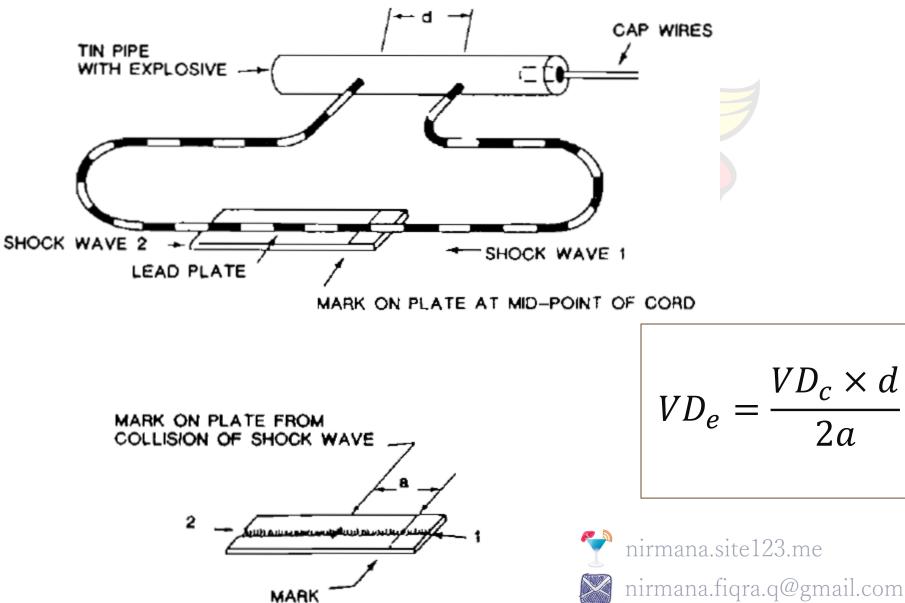
D'Autriche Method This method is based upon comparing the VD of the explosive with the velocity that is already

known of a detonating cord (VD_c). Therefore, the VOD_e of the explosive is determined from:

$$VD_e = \frac{VD_c \times d}{2a}$$



D'Autriche Method



Kodewimetro

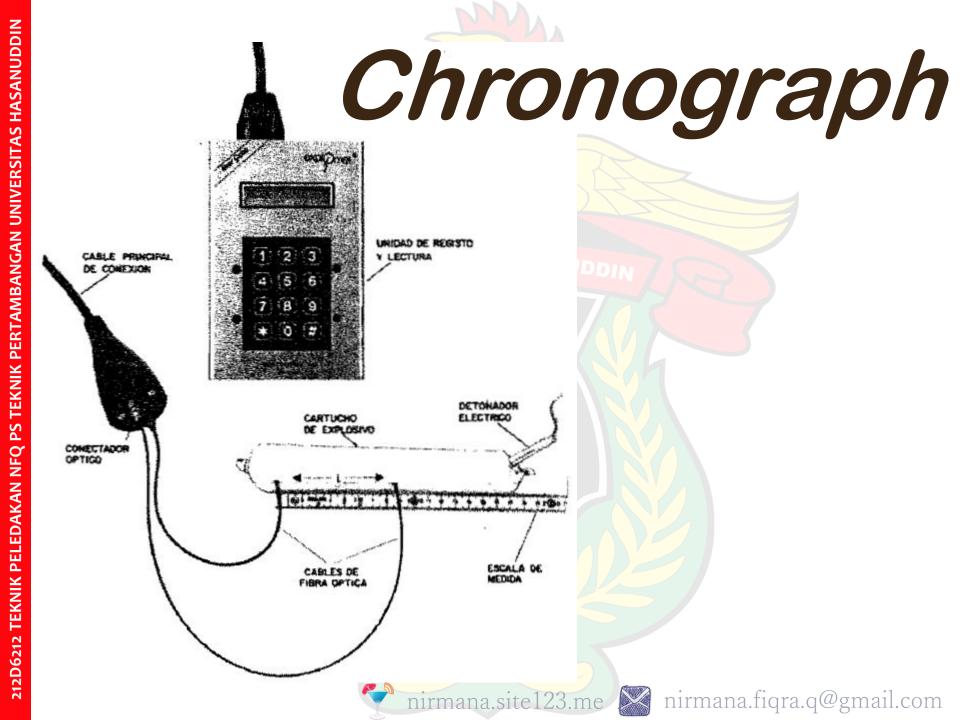
This is based upon the variation in resistance of a cable probe that goes through an explosive column axially. By means of special equipment called Kodewimetro, connected oscilloscope, the voltage variation, which to an İS proportional to the resistance, is measured while maintaining a constant current intensity in the circuit. As the detonation wave advances along the length of the explosive, the electric resistance diminishes and the VOD can be determined from the stress to which it is proportional.



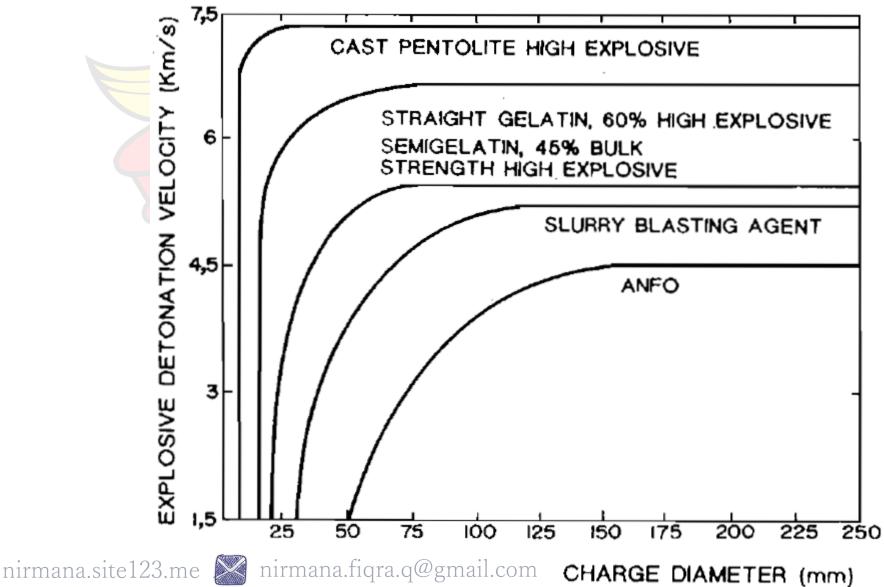
Chronograph

From two sensors introduced in the explosive and placed at a determined distance the VOD can be calculated by measuring the activation time of each sensor. At the moment, there are instruments that are capable of giving VOD directly and with high precision. The sensors can be electric or, more modernly, of optical fiber.

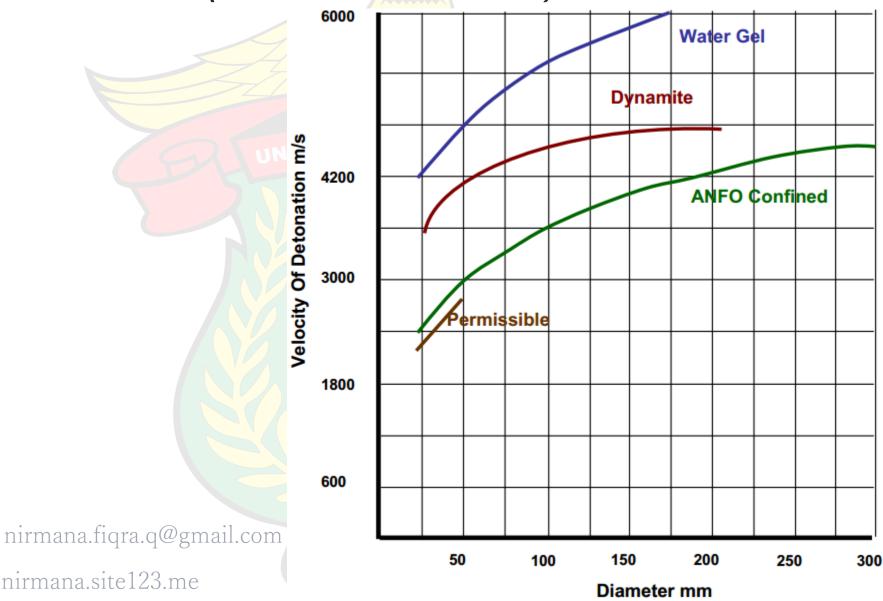




Influence of the charge diameter upon the detonation velocity (Ash, 1977)



Effect of explosive diameter on velocity of detonation (Bhandari, 1997)



Density	VOD (m/s)		
(gr/m ³)	De = 1.25 inch	De = 3 inch	De = 9 inch
0.8-1.4	2,240-6,080		
1.0-1.6	3,840-8,000		
1.1-1.3	4,160-6,080	4, <mark>480</mark> -6,080	
1.1 <mark>-1.6</mark>		<mark>4,480-6</mark> ,080	3,840-6,080
0.8-0.85	1,920-2,240	3,200-3,520	4,480-4,800
	(gr/m ³) 0.8-1.4 1.0-1.6 1.1-1.3 1.1-1.6	(gr/m³)De = 1.25 inch0.8-1.42,240-6,0801.0-1.63,840-8,0001.1-1.34,160-6,0801.1-1.60	(gr/m³)De = 1.25 inchDe = 3 inch0.8-1.42,240-6,0801.0-1.63,840-8,0001.1-1.34,160-6,0804,480-6,0801.1-1.64,480-6,080

3. Detonation Velocity (VOD) VOD (m/s) Density Type (gr/m^3) De = 1.25 inch De = 3 inch De = 9 inch Packaged 1.1-1.2 3,200-3,840 4,480-4,800 ANFO Heavy 1.1-1.4 3,520-6,080 ANFO





Every explosive also has a critical diameter which is the minimum diameter at which the detonation process, once initiated, will support itself in the column. In diameters smaller than the critical diameter the detonation of the explosive will not be supported and will be extinguished.





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The density of an explosive is important because explosives are <u>purchased</u>, <u>stored</u>, <u>and used</u> on a **weight basis**.

The density of the majority of explosives varies between 0.8 and 1.6 g/cm³ and, <u>as in detonation</u> <u>velocity, the greater it is, the more breakage it</u> provides.

4. Density

In blasting agents, density can be a critical factor because, if it is very low, they become sensitive to the detonating cord which begins to initiate them before the detonation of the primer cartridge; on the other hand, if it is very high they can become insensitive and not detonate. That limit density is called **Death Density**.





Density is normally expressed in terms of specific gravity, which is the ratio of explosive density to water density.

The specific gravity of the explosive is *commonly* used as a tool to approximate strength.



Typical Specific Gravity Values for Explosive Products

Туре	Specific Gravity
Granular Dynamite	NUDDIN 0.8-1.4
Gelatin Dynamite	1.0-1.7
Cartridged Slurry	1.1-1.3
Bulk Slurry	1.1-1.6
Air Emplaced ANFO	0.8-1.0
Poured ANFO	0.8-0.9
Packaged ANFO	1.1-1.2
Heavy ANFO	1.1-1.4

Typical Specific Gravity Values for Explosive Products

Туре	Specific Gravity	
Watergels and emulsions	0.8-1.5	
Cast boosters	1.6	







The prime purpose in varying the density of commercial explosives is to enable the total energy charge in a borehole to meet particular field conditions.





In many cases, such as in mining hard ore and driving tunnels through hard rock it is necessary to use dense gelatins or high density blasting agents in order to break the burden.





In other instances, as in production of certain ore or stone where a high percentage of lump is desired, the charges are distributed in the borehole with low density gelatins or blasting agents.





In still others, as in quarrying, a high density explosive is sometimes used in the bottom of hole to ensure pulling the toe, while a bulkier one is used to obtain proper distribution of the charge.





A useful guide in designing a blast is to know approximately how many kilograms of explosive be loaded in one meter of borehole. can Because the density of water is 1.0 g/cm³, products loaded into holes containing water must have a density greater than 1.0 g/cm³ in order to sink.

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A useful expression of density is **loading density** (or **charge concentration**), which is <u>the weight of</u> <u>explosive per unit length of charge</u> at a specified diameter.

The **density** of an explosive determines <u>the</u> weight that can be loaded into a given column of borehole.

The lineal charge concentration q_1 (kg/m) in a blasthole of diameter D and a density ρ_e , is calculated from:

$$q_1 = 7.854 \times 10^{-4} \times \rho_e \times D^2$$

where $\rho_e = \exp[\text{osive density } (g/\text{cm}^3), \text{ and } D =$ charge diameter (mm).







 $de = 0.34 \times SG_e \times D_e^2$

where:

- = loading density (lbs/ft) de
- SG_e = specific gravity of the explosive
- = diameter of explosive (in) D_{e}







EXERCISE

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Determine the loading density of an explosive which has a charge diameter of 3 inches and a specific gravity of 1.2.





5. Detonation Pressure and Explosion Pressure

The detonation pressure of an explosive is a function of the density and of the square of the detonation velocity. It is measured when the detonation is propagated through the explosive column, as already indicated. The detonation pressure is generally considered as the pressure in the shock zone ahead of the reaction zone.





5. Detonation Pressure and Explosion Pressure

Although the detonation pressure of an explosive depends upon, apart from the density and the VOD, the ingredients of which it is composed, this parameter can be estimated from the following equation (Jimeno, C.L., et al. in *Drilling and Blasting of Rocks*, 1995):

 $PD = 432 \times 10^{-6} \times \rho_e \times \frac{VD^2}{1 + 0.8 \times \rho_e}$



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5. Detonation Pressure and Explosion Pressure

 VD^2 $PD = 432 \times 10^{-6} \times \rho_e \times \frac{1}{1 + 0.8 \times \rho_e}$

where: PD = detonation pressure (MPa), ρ_e = density of explosive (g/cm³), and VD detonation velocity (m/s).



5. Detonation Pressure and Explosion Pressure

In the book of *Engineering Rock Blasting* Operations (Bhandari, 1997), the detonation pressure can be approximated as follows: $P = 2.5 \rho \cdot V^2 \times 10^{-6}$ where P = detonation pressure (kilobars), $\rho =$

density (g/cm³), V = detonation velocity (m/s).





5. Detonation Pressure and Explosion Pressure

The commercial explosives have a PD that varies between 500 and 1,500 MPa.

Generally, in hard, very dense, and competent rocks the fragmentation is done more easily with high detonation pressure explosives, owing to the direct relationship that exists between this variable and the breakage mechanisms of the rock.





Detonation Pressure

Туре	Detonation Pressure (kbar)
Granular Dynamite	SITAS HASANUDDIN 20-70
Gelatin Dynamite	70-140
Cartridged Slurry	20-100
Bulk Slurry	20-100
Poured ANFO	7-45
Packaged ANFO	20-60
Heavy ANFO	20-90



5. Detonation Pressure and Explosion Pressure

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5. Detonation Pressure and Explosion Pressure

The *detonation pressure* is *different* from the explosion pressure, which is the pressure after adiabatic expansion back to the original explosive volume.

The **explosion** pressure is *theoretically* about 45% of the detonation pressure.





Borehole pressure is the theoretical pressure exerted on the borehole walls by the expanding gases of detonation after the chemical reaction has been completed, and before any expansion of the borehole wall has taken place.





When an explosive charge is *initiated*, first a shock wave is caused, and then the pressure wave in the reaction zone follows (detonation wave). In some publications, borehole pressure means the pressure at the wall of the blasthole, but in others the borehole pressure has the same meaning as detonation wave.



Borehole pressure is a function of confinement and the quantity and temperature of the gases of detonation. Borehole pressure is generally considered to play the dominant role in breaking most rocks and in displacing all types of rocks encountered in blasting. Borehole pressures for commercial products range from less than 10 to 60 kbar or more.



Some results for borehole pressures measured in both laboratory and field blasts can be seen in the book of *Rock Fracture and Blasting* (Zhang, 2016). Many AN-FO mixtures have borehole pressures *larger* than their detonation pressures. In most high explosives the *detonation pressure* is the greater.



In classical theory (ideal explosives), the borehole pressure is quoted as:

$$p_b = \frac{\rho_e c_d^2}{8} 10^{-6}$$
 (ideal *fully coupled* explosives)

where p_h is the borehole pressure in MPa, ρ_e is the density of the explosive in kg/m³, and c_d is the detonation velocity of the explosive in m/s.



6. Borehole Pressure coupling (explosive in blasthole): the degree

and quality of interaction (filling) of the explosive charge with the borehole volume and borehole wall. It is defined by the volume of explosive in relation to the total volume of the blasthole



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6. Borehole Pressure

decoupling: normally a separation by air between the surface of an explosive charge and the blasthole wall where it is charged or sections of the blasthole left uncharged



The borehole pressure using decoupled charges can with reasonable reliability be calculated according to the following formula:

$$p_b = \frac{\rho_e c_d^2}{8} \left[\sqrt{R_a} \frac{d_e}{d_b} \right]^k 10^{-6}$$

(non-ideal and *decoupled* explosives)





 $p_b = \frac{\rho_e c_d^2}{8} \left[\sqrt{R_a} \frac{d_e}{d_b} \right]^k 10^{-6}$

where p_b = borehole pressure (MPa); ρ_e = density of the explosive (kg/m³); c_d = velocity of detonation (m/s); R_a = axial *decoupling*, percentage of explosive column charged (%), d_e = diameter of the explosive after charging into the blasthole (m), k = a value which has to be determined experimentally on site (the value of k is ~ 2.6 according to Atlas Powder, 1987). nirmana.site123.me 🔀 nirmana.fiqra.q@gmail.com

axial decoupling: the ratio between the length or volume of the blasthole being charged to the total available length or volume for charge in a blasthole





7. Stability

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Explosives should be chemically stable and not decompose under normal atmospherical conditions. A method to check the stability is called the Abel test, which consists in heating a sample during a set time and at a specific temperature, observing the moment in which decomposition initiates. For example, nitroglycerine at 80° takes 20 minutes to decompose.



The stability of the explosives is one of the properties that is related to the maximum storage time of these substances, so that their effects in a blast will not be reduced.





8. Water Resistance

This is the capacity of an explosive product to withstand exposure to water without losing sensitivity or efficiency. Explosive products have two types of water resistance, internal and external.



Internal Water Resistance

Internal water resistance is defined as water resistance provided by the explosive composition itself. It varies with the composition of the explosive and is generally linked to the proportion of nitroglycerine or special additives that they contain; thus watergels, gelatin dynamites and emulsions are quite resistant to water.



External Water Resistance

External water resistance is provided not by the explosive materials itself, but by the packaging or cartridging into which the material is placed.





8. Water Resistance

The emission of reddish-brown or yellow fumes from a blast often indicates inefficient detonation frequently reactions caused by water deterioration of the explosive.



8. Water Resistance

Manufacturers can describe the water resistance of a product in two different ways. One way would be using terms of classification generally accepted goes from Null (has no resistance to water), Limited, Fair, Good, Very Good, to Excellent (guarantees a resistance of more than 12 hours).

Water Resistance

Туре	Resistance	
Granular Dynamite	Poor to good	
Gelatin Dynamite	Good to excellent	
Cartridged Slurry	Very good	
Bulk Slurry	Very good	
Air Emplaced ANFO	Poor	
Poured ANFO	Poor	
Packaged ANFO	Very good (becomes poor if package is broken)	
Heavy ANFO	Poor to very good	
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Required Water Resistance in Different Blasting Operations

Blasting Operations	Required Water Resistance
Water is encountered in blasting operations	At least fair and should be detonated as soon as
	possible after loading
The explosive is to be in water for an appreciable amount of time	<i>At least</i> good
Severe (intense) water conditions and the exposure time is significant	Excellent
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8. Water Resistance

Other way ratings would have been given numbers.

Classification	Prolonged exposure to water with no detrimental effects
Class 1	72 hours
Class 2	48 hours
Class 3	24 hours
Class 4	12 hours





8. Water Resistance

In general, product price is related to water resistance. The more water resistant the product, the higher the cost.





9. Sensitivity

This characteristic globally envolves various meanings that depend upon the type of external action that affects the explosive.





9. Sensitivity

□ Controlled action: the sensitivity is equivalent to the acceptance of detonation by an initiator (e.g. electric blasting cap); sensitiveness Uncontrolled action: the sensitivity is a measure of the ease with which an explosive can be detonated by heat, friction, impact, or shock.



Cap Sensitivity (Sensitiveness) Explosives should be sufficiently sensitive to detonation by an adequate initiator. This capacity varies depending upon the type of product. As an example, the majority of gelatin explosives are initiated by *electric blasting caps*, whereas

blasting agents generally require a multiplier or primer of higher pressure and detonation velocity.





Cap Sensitivity

One of the classifications used is the following:

Explosives that are No. 8 cap sensitive; and

those that are not (*non cap sensitive*).

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Sensitivity to Shock or Friction

Some explosives can detonate by means of subsonic stimulants such as shock or friction. For safety purposes it is important to know their degree of sensitivity when faced by these especially during handling actions, and transportation.



Shock resistance test

It is usually carried out with a *drop hammer* (Kast), which consists in placing a sample of the product on an anvil, around 0.1 g, upon which a steel weight of 0.5 to 10 kg is dropped from different heights until explosion is achieved and a drop distance established.





Shock resistance test

For example, with a hammer of 2 kg, mercury fulminate detonates with a drop distance of 1 to 2 cm, nitroglycerine with 4 to 5 cm, dynamite with 15 to 30 cm, and ammonical explosives have drop distances of 40 to 50 cm.



Friction test

The most common is the Julius Peter test, in which an explosive is subjected to a friction process between two porcelain surfaces that have not been polished and upon which different pressures are exerted.



Friction test

After the test, any carbonization is noticeable as well as deflagration or explosion. The results are expressed in kilos which correspond to the pressure with which porcelain surface rubs upon the plate where the explosive is deposited.



Sensitivity to Heat

When explosives are heated gradually, they arrive at a temperature in which they suddenly decompose with release of gases, increasing little by little until finally a deflagration is produced or a small explosion. That temperature is called **Ignition Point**. In *black powder* it varies between 300 and 350°C, and in industrial explosives between 180 and 230 °C. This characteristic is <u>different</u> from sensitivity to fire, which *indicates* inflammable properties.





Critical Diameter

Cylindrical shaped explosive charges have <u>diameters</u> *below* which the detonation wave does not propagate or, if it does, it is with a velocity below the standard rate. This diameter is called **Critical Diameter**. The <u>principal factors</u> that influence the critical diameter

of an explosive are: particle size, the reactivity of its components, the density, and the confinement of said components.

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Sensitivity 9.

Туре	Hazard Sensitivity	Performance Sensitivity
Granular Dynamite	Moderate to high	Excellent
Gelatin Dynamite	Moderate	Excellent
Cartridged Slurry	Low	Good to very good
Bulk Slurry	Low	Good to very good
Air Emplaced ANFO	Low	Poor to good*
Poured ANFO	Low	Poor to good*
Packaged ANFO	Low	Good to very good
Heavy ANFO	Low	Poor to good*

* Heavily dependent on field condition





Sympathetic transmission is the phenomenon produced when a cartridge, upon detonation, induces the explosion of another that İS adjacent.



A good transmission within the blastholes is the guarantee that the explosive columns will be <u>completely detonated</u>. *However,* when those blastholes are close, or the charges within are decked, a sympathetic detonation can be produced by transmission of the strain wave through the rock, by the presence of underground water and structural discontinuities, or by pressure of the inert material of intermediate stemming upon the adjacent charges. In all these cases the results of fragmentation and vibrations would be seriously damaged.



One of methods to measure the capacity or aptitude for sympathetic detonation, also defined as the *Coefficient* of Autostimulation, consists in calculating the maximum distance at which a primed cartridge can make another non-primed receiver cartridge explode, both being aligned with reference to their axis and well in contact with a ground or metal surface, or even inside tubes of different materials or in the open air.



In the majority of the industrial explosives, the maximum distances at which sympathetic detonation is produced are between 2 and 8 times their diameter, depending upon the type of explosive.



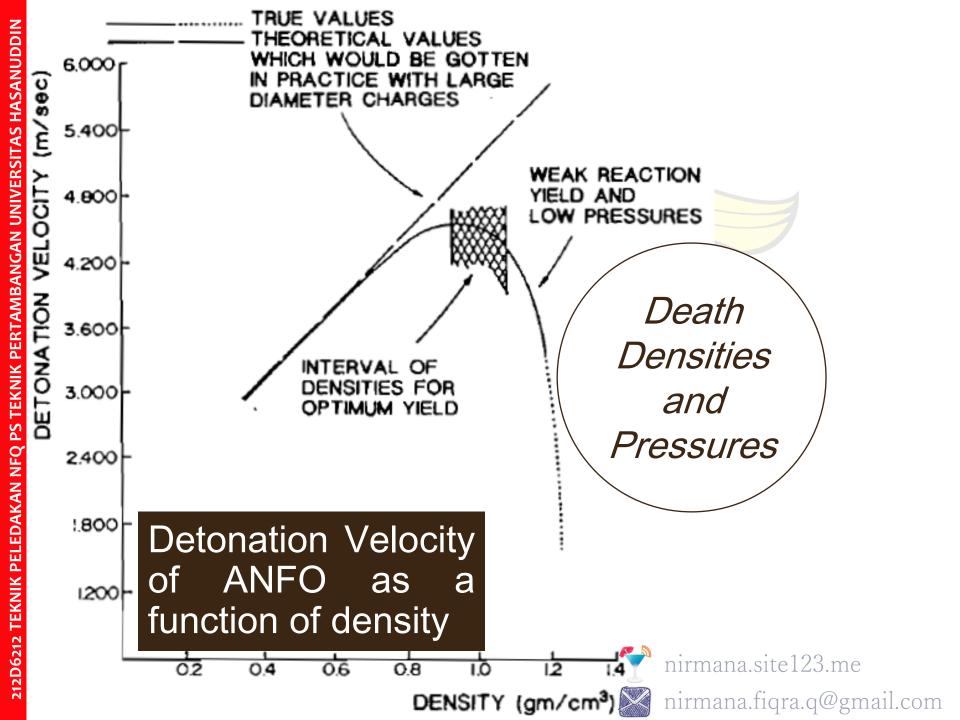
The measures of the Autostimulation Coefficient can be taken either directly or indirectly; however, in the second, only 50% of the energy given by the direct method is transmitted. The factors which modify the results of these tests are: aging, the calibre of the cartridges and the method used in testing.



11. Desensitization

In many industrial explosives it has been observed that the sensitivity diminishes when the density increases beyond a certain value. This phenomenon is more acute in those compositions or blasting agents that do not contain substances such as TNT or Nitroglycerine, etc.





12. Temperature Resistance

Explosive compounds can suffer (appear worse in quality) in performance if stored under extremely hot or cold conditions.

Under hot storage conditions, above 90°F, many compounds will slowly decompose or change properties and shelf life will be decreased.



12. Temperature Resistance

When the environmental temperature is under 8°C, the explosives which contain nitroglycerine tend to freeze. By adding a certain amount of nitroglycol, the freezing temperature is lowered to -20°C.



12. Temperature Resistance

Туре	Between 0-100°F
Granular Dynamite	Good
Gelatin Dynamite	Good
Cartridged Slurry	Poor below 40°F
Bulk Slurry	Poor below 40°F
Air Emplaced ANFO	Poor above 90°F
Poured ANFO	Poor above 90°F
Packaged ANFO	Poor above 90°F
Heavy ANFO	Poor below 40°F







The detonation of any commercial explosive produces steam, nitrogen, carbon dioxide, and eventually, solids and liquids.

Among the harmless gases mentioned, there is always a certain percentage of toxic gases such a carbon monoxide and nitrogen oxides. These resulting products are called fumes.







If there is insufficient oxygen (a negative oxygen balance), the tendency to form carbon monoxide is increased. If there is an excess of oxygen (a positive oxygen balance), oxides of nitrogen are formed.







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The weight of <u>paper and wax</u> per cartridge affects oxygen balance and this <u>must be considered</u> in the calculation.

Because oxygen has such an important effect on the types of gases evolved, it is closely controlled in formulation. **Oxygen balance** is kept within specific limits to give the lowest practical content of toxic gases.



- Poor product formulations
- ✓ Insufficient charge diameter
- ✓ Inadequate priming or initiation
- ✓ Water deterioration
- ✓ Lack of confinement
- ✓ The use of plastic borehole





According to the proportion of harmful gases, a

scale of classification has been established in

degrees of toxicity for the operators after blasting.

Class	Volume of toxic gases (CO-NO ₂) dm ³ per 200 g of explosive	Usage
1	0-4.53	Any type of UG work
2	4.53-9.34	Well ventilated areas
3	9.34-18.96	Surface blastings





- Maximum Allowable Concentrations (peak values) acceptable in general are:
- ✓ Carbon Monoxide, 50 ppm;
- ✓ Nitrogen Dioxide, 5 ppm.





Туре	Quality Relating Fume	
Granular Dynamite	Poor to good	
Gelatin Dynamite	Fair to very good	
Cartridged Slurry	Good to very good	
Bulk Slurry	Fair to very good	
Air Emplaced ANFO	Good*	
Poured ANFO	Good*	
Packaged ANFO	Good to very good	
Heavy ANFO	Good*	

* Can be poor under adverse conditions





There are several ways to determine fume concentrations. These include: measurements in the Bichel gauge, the Crawshaw-Jones Apparatus, the Ardeer Tank, field tests and theoretical calculations (Bhandari, 1997 in Engineering Rock Blasting Operations).





The *most efficient* method is to take on-site measurements after the blast. A rather simplified approach is that of using spot samplers for detecting concentration of gases.





